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# Design guidelines for direct ground cooling systems in different climates

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# Outline

- introduction to direct ground cooling systems – research scope
- methodology
- system layout, reference building, climates
- dynamic simulations in different climates, by varying the building size and the envelope thermal properties
- GHEx design criteria and discussion

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## Direct ground cooling systems

Cooling is achieved through water circulation between radiant panels in the building and a ground heat exchanger

The ground heat exchanger sizing is a critical issue:

- oversizing → high costs
- undersizing → low performance

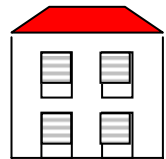
Existing guidelines and methods focus on ground coupled heat pumps and heating use [VDI 4640, Kavanaugh..] → application to direct ground cooling systems not straightforward (sensitivity to ground temperature levels...)

In this study: dynamic simulations → preliminary criteria for direct ground cooling systems sizing in the Italian climates (influencing the ground temperature and the building cooling demand)

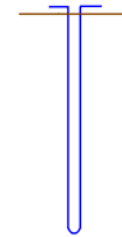
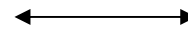
# Methodology 1/3

	$\langle T \rangle$ (°C)	Tmin (°C)	Tmax (°C)
Milano	11.8	-10.0	32.6
Roma	15.8	-4.0	31.8
Palermo	18.8	4.8	34.0

Modifying  
the envelope  
(A, B, C)



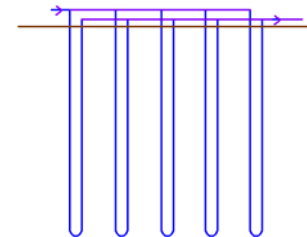
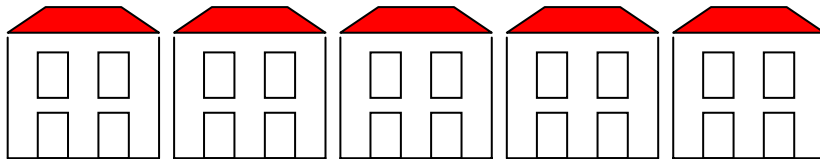
Varying the  
climate



Finding the  
GHEX size

Scaling the  
building size  
x10, x100

Scaling the  
GHEX size...

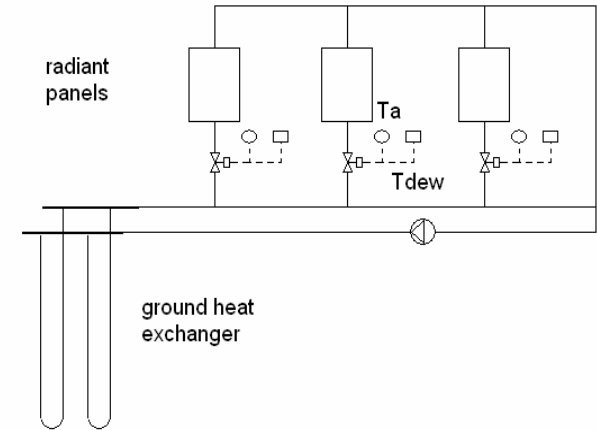


# Methodology 2/3

## ■ Direct ground cooling system:

- ✓ vertical GHEX (one U pipe per borehole - average ground thermal properties)
- ✓ chilled floors;
- ✓ room thermostats and dew point sensors;
- ✓ operating from June to September for 30 years.

■ **Reference building:** two storey single family house



	Envelope A	
	U W/m <sup>2</sup> K	g
External walls	0.46	
Roof	0.82	
Floor on ground	0.64	
Windows	3.28	0.76
Shading	Not present	

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## Methodology 3/3

Long term evaluation of summer comfort conditions through TRNSYS simulations:

- for each summer calculation of  $\langle \text{PMV} \rangle$  and mean standard deviation  $\Delta$
- adjusting the GHEx size (N, H, d) in order to have, throughout the 30 years:

$$\langle \text{PMV} \rangle + \Delta \leq 0.5$$

comfort level (1)

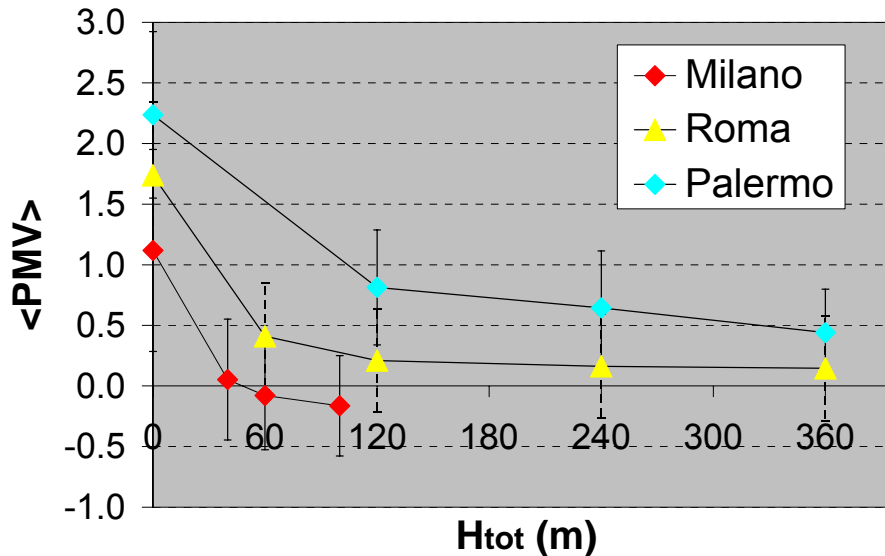
(Class B environment EN 7730)

or, if the previous condition is too hard to reach,:

$$\langle \text{PMV} \rangle + \Delta \leq 0.8$$

comfort level (2)

# Simulations / building x1



- in Milano  $N=1$   $H=60$  m is enough;  $Q_{30y}/Q_{1y} = 96\%$

- in Roma and Palermo  $H_{tot}=360$  m is not enough! Condensation prevention is partially responsible for that!

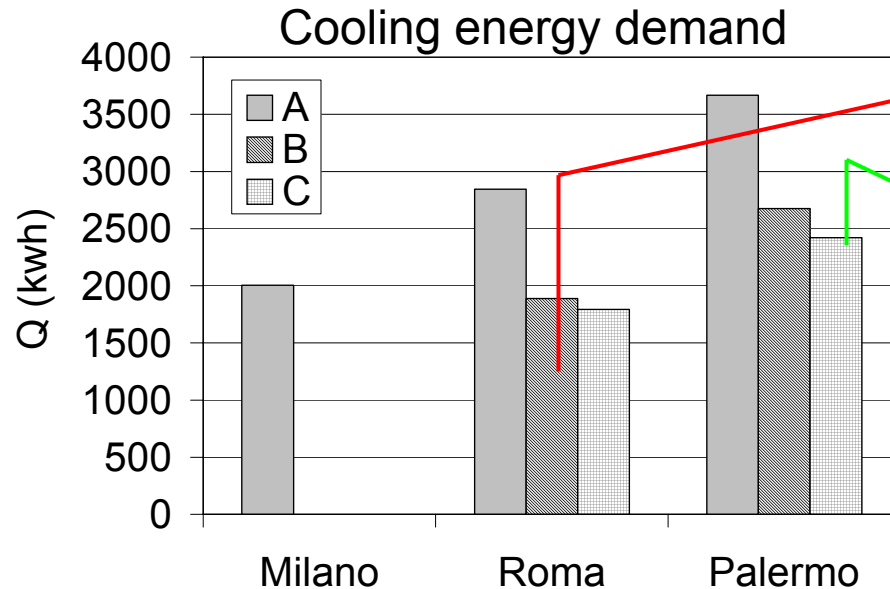
- What happens if we:

- apply a solar control strategy (*envelope B*)

- and increase the thermal insulation? (*envelope C*)

	Envelope A		Envelope B		Envelope C	
	U W/m <sup>2</sup> K	g	U W/m <sup>2</sup> K	g	U W/m <sup>2</sup> K	g
External walls	0.46		0.46		0.24	
Roof	0.82		0.82		0.24	
Floor on ground	0.64		0.64		0.64	
Windows	3.28	0.76	1.74	0.39	1.74	0.39
Shading	Not present		Overhangs		Overhangs	

# Simulations / building x1



Roma envelope B c.l.(1):  
N=1 H=70 m

Palermo envelope C c.l.(1):  
 $H_{\text{tot}}=450$  m not enough!

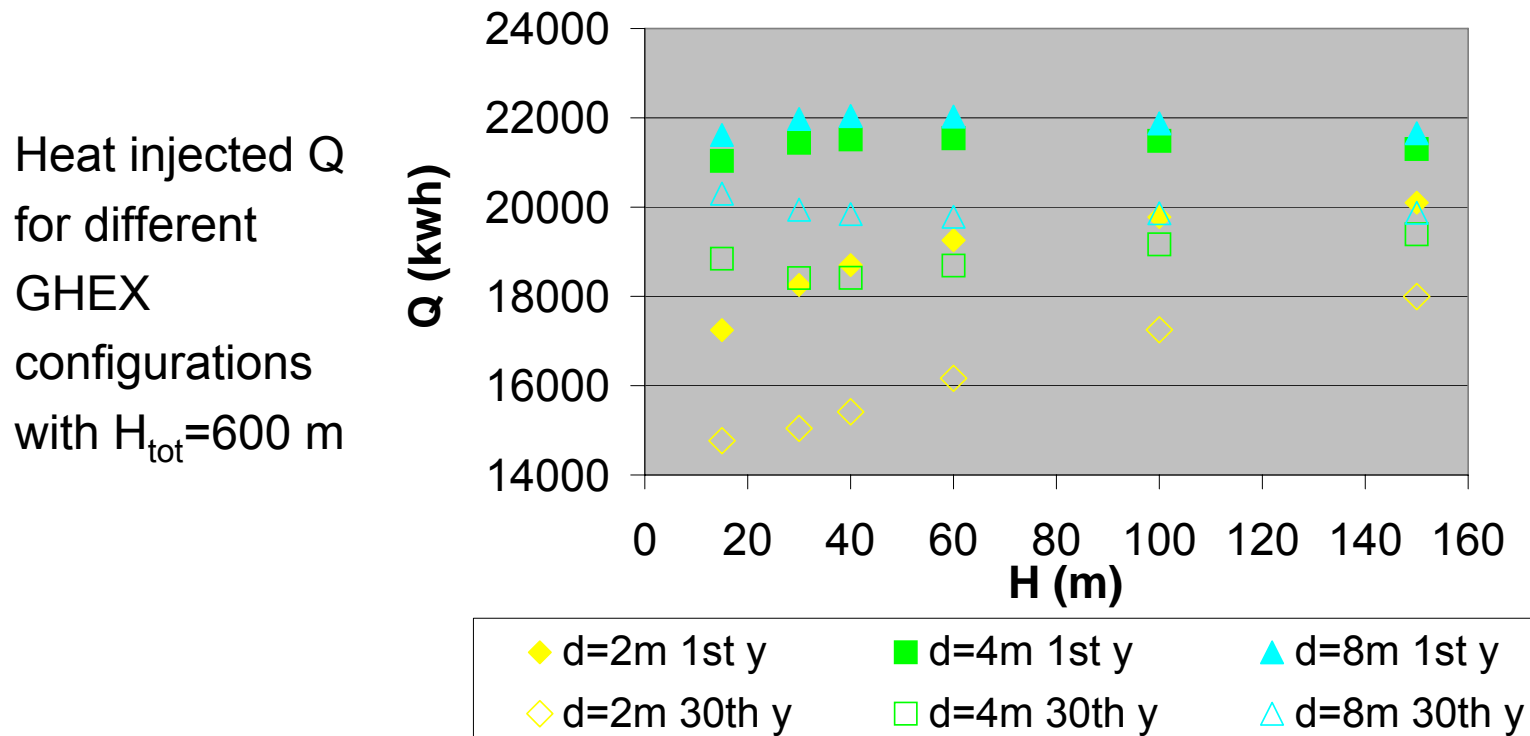
moving to c.l.(2):  
N=2 H=90 m  $d \geq 2$  m

Climate	envelope	comfort level	$H_{\text{tot}}$ (m)	Configuration
Mi	A	(1)	60	N=1 H=60m
Ro	B	(1)	70	N=1 H=70m
Pa	C	(2)	180	N=2 H=90m $d \geq 2$ m

# Simulations / building x10

Milano: envelope A c.l. (1)

$H_{\text{tot}}=60\text{m} \times 10= 600 \text{ m}$  is ok but...if the boreholes distance  $d$  is too short the system performance decreases significantly with time!



# Simulations / building x10

Roma envelope B c.l.(1):

$H_{tot}=70 \text{ m} \times 10=700 \text{ m}$  is found to be insufficient, even if  $d=20 \text{ m}$ !

→  $H_{tot}=1000 \text{ m}$  with  $d \geq 8 \text{ m}$

Palermo envelope C c.l.(2):

$H_{tot}=180 \text{ m} \times 10=1800 \text{ m}$  is ok if:

- $d \geq 8 \text{ m}$ ,  $H=15 \text{ m}$
- $d \geq 16 \text{ m}$ ,  $H=150 \text{ m}$

climate	env.	comf. level	$H_{tot}$ (m)	configurations	
				d	H, N
Mi	A	(1)	600	$\geq 8 \text{ m}$	H=15÷150m N=40÷4
				4 m	H=15m N=40; H=100m N=6; H=150m N=4;
Ro	B	(1)	1000	$\geq 8 \text{ m}$	H=20÷150m N=50÷7
Pa	C	(2)	1800	$\geq 8 \text{ m}$	H=20m N=90
				$\geq 16 \text{ m}$	H=90m N=20
			3000	$\geq 8 \text{ m}$	H=120m N=25
				$\geq 8 \text{ m}$	H=90m N=33

# Simulations / building x100

climate	env.	comf. level	H <sub>tot</sub> (m)	Configurations	
				d	H, N
Mi	A	(1)	6000	≥8 m	H=15m N=400
				≥16m	H=100m N=60
			9000	≥8 m	H=30m N=300 H=60m N=150
Ro	B	(1)	10.000	≥8 m	H=20m N=500
				≥20m	H=100m N=100
			15.000	≥12 m	H=100m N=150
Pa	C	(2)	18.000	≥12 m	H=20m N=900
				≥20 m	H=90m N=200
			30.000	≥16 m	H=120m N=250
				≥ 8 m	H=30m N=1000

In order to scale the GHEX size according to the buildings', large d or little H are required

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## Conclusions

- in warm-humid climates the need to avoid condensation on chilled surfaces may limit the cooling system performance
- the direct ground cooling system size strongly depends on the envelope thermal properties
- the GHEX size is very sensitive to the ground temperature level
- in small scale GHEX with few boreholes the system long term operation is stable
- in medium and large scale GHEX thermal interactions between neighbour boreholes and heat injection year after year may reduce the system performance:
  - ✓ a larger interaxial distance is required;
  - ✓ total boreholes length being equal, best long term behaviour is found for shallow configurations, since their aspect ratio permits natural ground recharge in winter by heat transfer with outside air.