

Journée du CUEPE 2006 Geneva, 6th of April 2006



Magnetic heating and refrigeration: A new technology of heat and cold production

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Collaboration and Help



New name:

heig-vd

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"Giant" magnetocaloric effect



New materials ... may bring practical magnetocaloric cooling a step closer. A large magnetic entropy change has been found to occur in $MnFeP_{0.45} As_{0.55}$ at room temperature, making it an attractive candidate for commercial applications in magnetic refrigeration.

Nature Highlights 10 th of January 2002



"Giant" magnetocaloric effect



In an article published in the journal *Nature* last month, scientists at the University of Amsterdam reported that they had created an iron-based compound that also exhibits a large warming effect in a magnetic field. Iron and other ingredients in the compound are considerable less expensive than gadolinium.

> The New York Times 9 th of February 2002



"Giant" magnetocaloric effect







Brief history of magnetocaloric materials and systems



- 1881 : Warburg discovers the magnetocaloric effect in iron
- 1926 : Debye proposes the first practical application at low temperatures. The process is named adiabatic magnetization/demagnetization
- 1927 : Giauque proposes the same process independently of Debye
- Since 1930 : Application of magnetic cooling becomes standard in low temperature physics (T<<1 K)
- At present : Discovery of magnetocaloric materials with Currie temperatures T_C around room temperature
- Development of new magnetic cooling systems operating at room temperature: **Promising new technology !**





For the entropy of rare earth alloys (no electron phonon interactions) a superposition of the partial entropies is possible (Tishin, 2003): $S(H,T)=S_{\rho}(T)+S_{I}(T)+S_{m}(H,T)$

The entropy of the electronic (e) and the lattice (l) subsystems show no dependence on the magnetic field! Then:

$$ds(H,T) = \frac{ds_e}{dT}(T)dT + \frac{ds_l}{dT}(T)dT + \left(\frac{\partial s_m}{\partial H}\right)_T (H,T)dH + \left(\frac{\partial s_m}{\partial T}\right)_H (H,T)dT$$

Some basic thermodynamic relations and definitions:

$$\delta q = T ds$$
 $c_{\chi} = \left(\frac{\delta q}{\partial T}\right)_{\chi}$ $c_{\chi} = T \left(\frac{\delta s}{\partial T}\right)_{\chi}$





Combining these equations:

$$ds(H,T) = \frac{c_e(T)}{T} dT + \frac{c_l(T)}{T} dT + \frac{c_m(H,T)}{T} \bigg|_H dT + \left(\frac{\partial s_m}{\partial H}\right)_T (H,T) dH$$

With the Mayxwell relation (e.g. Kitanovski & Egolf, Int. J. Refr. **29**, 3-21, 2006:

$$\left(\frac{\delta s}{\partial H}\right)_T = -\mu_0 \left(\frac{\delta M}{\partial T}\right)_H \qquad \text{because:} \qquad \left(\frac{\delta s}{\partial H}\right)_T = \left(\frac{\delta s}{\partial H}\right)_T$$





and:

 $c_H = c_e + c_l + c_m$

In an adiabatic magnetization or demagnetization process:

ds=0

Therefore, it follows that:



Moving magnetocaloric material into (out of) a magnetic field increases (decreases) the magnetisation and the temperature.





The magnetocaloric effect occurs at a phase transition between different magnetic states.

The temperature of phase change is the Curie temperature.







Data from:

Pecharsky VK, Gschneidner KA Jr. *Tunable magnetic regenerator alloys with a giant magnetocaloric effect for magnetic refrigeration from* ~ 20 to ~ 290 K. Applied Physics Letters 1997; 70 (24): 3299-3301.

Still limited temperature differences!



Magnetic heating and refrigeration at room temperature







Heating and refrigeration ,, capacities ":



Tegus et al., 2002

Zimm et al., 2001



Magnetocaloric materials should (partly by Yu et al., 2003):

- Modest Debye temperature (a high temperature makes the fraction of lattice entropy small correspondingly at a high temperature)
- High temperature difference at phase transition
- Large width of transition
- No magnetic hysteresis (irreversibility of cycle)
- Small specific heat and large thermal conductivity to guarantee fast heat exchange
- Large electric resistance to avoid the eddy current loss
- Fine molding and processing must be possible
- No poison substances (arsenic, etc.) for direct contact applications









High flux line density



Magnetic heating and refrigeration at room temperature





Four stage process each:

A) Magnetic heat pump:

- 1) Increase of magnetic flux density
- 2) Rejection of heat for heating purpose at high temperature level
- 3) Decrease of magnetic flux density
- 4) Injection of heat at low level to the heat pump

B) Conventional heat pump:

- 1) Compression (Increase of pressure)
- 2) Rejection of heat for heating purpose at high temperature level
- 3) Expansion (decrease of pressure)
- 4) Injection of heat at low level to the heat pump





Advantages:

- Green technology (no use of conventional refrigerants)
- Noise-less technology (no compressor)
- Very high thermodynamic efficiency (20-30% higher than in conventional cycles due to the reversibility of the magnetocaloric effect)
- Lower energy consumption
- Simple construction
- Low maintenance costs
- Low pressures (operation at atmospheric pressure, advantage e.g. for air-conditioning applications and refrigeration systems in automobiles)



Disadvantages:

- Strong magnetic fields with not completely known influences on living creatures
- Protections to avoid disturbances of electronic components
- The field strengths of permanent magnets are still limited, superconducting magnets are too expensive
- The temperature differences are still not so high
- In moving material applications the precision of the machine must be high (small gap between magnet and magnetocaloric material)







A development in Japan

Chubu – Toshiba (2000)

This machine consists of a cascade with three pistons of different magnetocaloric materials. A low magnetic field of B=0.7 T is induced by permanent magnets.







Development in the USA

AMES Laboratory - 1997

The kernel are two pistons of packed beds of gadolinium spheres. A superconducting magnet with a high magnetic field is applied.





Development in the USA

AMES Laboratory - 2001







Rotary magnetic refrigerator with permanent magnets (with complicated fluid switches)







Developments in the USA

University of Victoria





Magnetic forces and thermodynamic potentials





Dilute limite only (ferrofluids)!

Kitanovski & Egolf, 2005 (in print)



Magnetic forces and thermodynamic potentials





What is the difference?

We still may have the external work:

 $dw_1^{(ext)} = -\mu_0 H_0 dM$

But now additionally a flux of magnetisation occurs. Its infinitesimal change is:

$$dw_1^{(abs)} = -\mu_0 d(H_0 M)$$

Then the technical work is:

$$dw_1^{(tech)} = -(dw_1^{(abs)} - dw_1^{(ext)}) = \mu_0 M dH_0$$

In turbo machinery this work is also named shaft work



Magnetic forces and thermodynamic potentials



Quantity	Gas thermodynamics	Magneto- thermodynamics
Driving "force" (stress parameter)	Pressure <i>p</i>	Field <u>H₀</u>
Order parameter (reaction of system)	Specific volume v	Magnetization <i>M</i> (orientation of spins)
External work (closed system)	$\frac{dw_1^{(ext)}}{dw_1} = -pdv$	$\frac{dw_1^{(ext)} = -\mu_0 H_0 dM}{(related to force of Liu)}$
Technical work (open system)	$dw_1^{(tech)} = vdp$	$\frac{dw_1^{(tech)} = \mu_0 M dH_0}{(related to Kelvin force)}$



Possible Systems







Possible systems: Open systems







Possible systems



- 1) Static system with two storage blocks and valves
- 2) Linear movement
- 3) Rotational movement

Solution A: Rotary wheel, magnet fixed, axial current.



Solution C: Rotary wheel, fixed magnet, radial current.



Solution B: Wheel fixed, rotating magnet, axial current.



Solution D: Fixed wheel, rotary magnet, radial current.





Porous rotary magnetic refrigerator





A. Kitanovski, P. W. Egolf, O. Sari, 2003. *Procédé et dispositif pour generer en continue du froid et de la chaleur par effet magnetique.*

PCT BR – 10'463 - IN

Four functions are realized in a very simple manner!





Thermodynamic cycles, cascades, regeneration





A. Kitanovski, P.W. Egolf H₀⁽²⁾ > H₀⁽¹⁾ International Journal of Refrigeration *Thermodynamics of Magnetic Refrigeration* (in print):

Internal energy:

$$du_1 = T ds - \mu_0 \vec{H}_0 d\vec{M}$$

Legendre Transformation:

$$h_1 = u_1 + \mu_0 \vec{H}_0 \vec{M} \longrightarrow dh_1(s, H_0) = Tds + \mu_0 M dH_0$$

"Coefficient of performance":

$$COP_{Brayton} = \frac{\left[h^{(1)} - h^{(4)}\right]}{\left[h^{(2)} - h^{(1)}\right] + \left[h^{(4)} - h^{(3)}\right]}$$



Thermodynamic cycles, cascades, regeneration





To improve the available temperature differences cascade systems..







Thermodynamic cycles, cascades, regeneration



... or regeneration systems are required!







Numerical method and simulations



<u>n</u>

Energy conservation:

$$\rho\left(\frac{\partial\Lambda}{\partial t} + \omega\frac{\partial\Lambda}{\partial\phi} + v\frac{\partial\Lambda}{\partial z}\right) + \frac{1}{r}\frac{\sum_{i=1}^{r}\dot{q}_{\chi\phi}}{\partial\phi} + \frac{\sum_{i=1}^{r}\dot{q}_{\chiz}}{\partial z}$$

Mapping of a cylinder to a square:

Thermal inertia and conductivities negligible!

<u>n</u>

$$\begin{split} \rho_{F} v c_{p} \frac{\partial T_{F}}{\partial z} + & \frac{\alpha \xi}{L} (T_{F} - T_{R}) = 0 \\ \rho_{R} \omega c_{H} \frac{\partial T_{R}}{\partial \phi} \psi + & \frac{\alpha}{\delta} (T_{R} - T_{F}) = 0 \end{split}$$

$$TF(\phi, L) = TF_{in}^{(hot)}, \quad TR(\phi, L) = TR_{in}^{(hot)} + \Delta T^{(hot)}, \quad \pi < \phi \le 2\pi$$

$$TF(\phi, 0) = TF_{in}^{(cold)}, \quad TR(\phi, 0) = TR_{in}^{(cold)} + \Delta T^{(cold)}, \quad 0 < \phi \le \pi$$

$$TR(2\pi, z) = TR(0, z), \quad 0 \le z \le L \qquad (Periodicity condition)$$



Numerical method and simulations





Temperature distributions in a steady state condition: L=0.2 m, D=0.198 m., $v_{cold}=v_{warm}=6 \text{ m/s}$, $\omega=0.6 \text{ s}^{-1}$, $\dot{Q}=704 \text{ W}$, $m_{wheel}=8.09 \text{ kg}$, $\Delta B=5 \text{ Tesla}$. Material: $\text{Gd}_5(\text{Si}_{1.985}\text{Ge}_{1.985}\text{Ga}_{0.03})$



Newest work: Analytical optimization





More simple (also analytical) models:

$$\chi_{R} = \frac{h}{\psi \ \delta \ \rho_{R} \ f \ c_{H}} = \frac{1}{\psi} \frac{L}{\delta} \frac{St_{R}}{S_{r}},$$

$$St_{R} = \frac{h}{\rho_{R} \ c_{H} \ \nu}, \qquad S_{r} = \frac{f \ L}{\nu} << 1$$

$$\chi_F = \frac{h \xi}{\rho_F v c_{pF}} = \xi St_F = NTU ,$$

$$St_F = \frac{h}{\rho_F c_{pF} v}$$

$$COP = \frac{1}{2} \underbrace{\frac{\chi_{R}^{(hot)}}{\chi_{F}^{(hot)}} \left(1 - e^{-\chi_{F}^{(hot)}}\right)}_{\leq 1} \left(1 - \frac{T_{F, in}^{(hot)}}{T_{R}^{(hot)}}\right) COP_{Carnot} , \qquad COP_{Carnot} = \frac{T_{R}^{(hot)}}{T_{R}^{(hot)} - T_{R}^{(cold)}}$$



Numerical method and simulations









Numerical method and simulations





Color Shade Results Quantity : |Flux density| Tesla

0 / 156.25E-3 156.25E-3 / 312.5E-3 312.5E-3 / 468.75E-3 468.75E-3 / 0.625 0.625 / 781.25E-3 781.25E-3 / 937.5E-3 937.5E-3 / 1.09375 1.09375 / 1.25 1.25 / 1.40625 1.40625 / 1.5625 1.5625 / 1.71875 1.71875 / 1.875 1.875 / 2.03125 2.03125 / 2.1875 2.1875 / 2.34375 2.34375 / 2.5

Ferromagnetic kernel



Alternative machines





Second generation of a rotative prototype with regeneration.



Alternative machines





A system with radial flow is being built and will be presented at the Hannover industrial exhibition 2006.



Heat pumps for new buildings with floor heating

Fluids:Brine/Temperature primary side:0 °C (Temperature secondary side:35 °CPower:8 kW

Brine/water (brine: 25 % ethylen-glycol) 0 °C (e.g. water of a river) 35 °C 8 kW

Renovation building with radiator heating

Fluids:Air/waterTemperature primary side :-7 °CTemperature secondary side :50 °CPower:15 kW.







Conventional heat pump application

Analogous design of a magnetic heat pump



Simple magnetic heat pump system with only two pumps. A requirement is identical fluids in the two circuits, e.g. water/glycol.









Schematic drawing of a complete heating system with a magnetic heat pump. By the heat recovery system the required temperature difference becomes smaller and a magnetic heat pump appplication becomes realistic.



New IIR Working Party on Magnetic Refrigeration





See on the web: www.iifiir.iifiir.org



First Int. Conf. on Magnetic Refrigeration at Room Temperature





27-30. September 2005 in Montreux Switzerland

Interested: Coca Cola, Néstle, Daewoo, Danfoss, Peugeot, Citroen, Axima, Arcelik,...

Next conference: Protorosz, Slovenia 11-13 April 2007



Swiss Technology Award 2006 First prize







Conclusions and Outlook



- Magnetic refrigerators at room temperature have been designed (and several patents for different systems submitted)
- The basic theory has been established, but will be further prepared
- First numerical simulations results have been made available
- Experimental validation is planned to be performed
- Optimisation calculations are very important to reach high COP values and are still missing
- More powerful systems as cascades and systems with regeneration must be designed, their behaviour measured and modeled.



Thank you for your attention!





Magnetic cooling at room temperature:

A future major evolution in refrigeration?